

## Virtual Temperature

In atmospheric thermodynamics, the virtual temperature ( $T_v$ ) of a moist air parcel is the temperature at which a theoretical dry air parcel would have as total pressure and density equal to the moist parcel of air.

### 上节课回顾

Consider a moist air parcel containing masses  $m_d$  and  $m_v$  of dry air and water vapor in a given volume  $V$ . The density is given by

$$\rho = \frac{m_d + m_v}{V} = \rho_d + \rho_v,$$

where  $\rho_d$  and  $\rho_v$  are the densities the dry air and water vapor would respectively have when occupying the volume of the air parcel.

Rearranging the standard ideal gas equation with these variables gives

$$e = \rho_v R_v T \text{ and } p_d = \rho_d R_d T.$$

Solving for the densities in each equation and combining with the law of partial pressures yields

$$\rho = \frac{p - e}{R_d T} + \frac{e}{R_v T}.$$

Then, solving for  $p$  and using  $\epsilon = \frac{R_d}{R_v} = \frac{M_v}{M_d}$  is approximately 0.622 in Earth's atmosphere:

$$p = \rho R_d T_v,$$

where the virtual temperature  $T_v$  is

$$T_v = \frac{T}{1 - \frac{e}{p}(1 - \epsilon)}.$$

We now have a non-linear **scalar** for temperature dependent purely on the **unitless** value  $e/p$ , allowing for varying amounts of water vapor in an air parcel. This virtual temperature  $T_v$  in units of **kelvin** can be used seamlessly in any thermodynamic equation necessitating it.

# 2.2 浮力

## 上节课回顾

$$\frac{B}{g} \approx \frac{\theta'}{\bar{\theta}} + 0.61q_v' - \frac{c_v p'}{c_p \bar{p}} - q_h$$

升温1K对浮力的贡献相当于：  
 增加5–6 g/kg 的水汽  
 减小3–4 hPa的气压  
 减小 3.3 g/kg的Water loading

### (2) 不考虑凝结水、混合、扰动气压的作用(气块法)

$$\frac{B}{g} \approx \frac{\theta'}{\bar{\theta}} = \frac{T'}{\bar{T}} = \frac{T_p - T_e}{T_e}$$

$$B \approx g \frac{T_p - T_e}{T_e}$$

气块法可能高估了浮力

$$\theta = T \left(\frac{p_0}{p}\right)^{R/c_p}$$

$$\frac{\theta'}{\bar{\theta}} = \frac{T'}{\bar{T}} - \frac{R}{c_p} \frac{p'}{\bar{p}}$$

# 2.3 静力稳定度分析

上节课回顾

$$c_p \frac{d\theta}{\theta} = \frac{1}{T} (c_p dT + g dz) \quad \text{两边除以 } c_p dz:$$

$$\frac{1}{\theta} \frac{d\theta}{dz} = \frac{1}{T} \left( \frac{dT}{dz} + \frac{g}{c_p} \right) \quad \text{对于平衡位置处的小扰动, 可近似为:}$$

$$\frac{1}{\theta_0} \frac{\Delta\bar{\theta}}{\Delta z} = \frac{1}{T_0} \left( \frac{\Delta T}{\Delta z} + \Gamma_d \right) \Rightarrow \frac{1}{\theta_0} \frac{\partial \bar{\theta}}{\partial z} = \frac{1}{T_0} (\Gamma_d - \gamma)$$

$$\text{因而 } \left[ \frac{g}{T_0} (\Gamma_p - \gamma) \right]^{1/2} = \left[ \frac{g}{\theta_0} \frac{\partial \bar{\theta}}{\partial z} \right]^{1/2} = N$$

$$\gamma < \Gamma_p \Rightarrow \frac{\partial \bar{\theta}}{\partial z} > 0$$

$$\text{饱和情况下, 振动频率为 } N_m = \left[ \frac{g}{\theta_e} \frac{\Gamma_m}{\Gamma_d} \frac{\partial \bar{\theta}_e^*}{\partial z} \right]^{1/2}$$

## 2.4 对流有效位能 CAPE

上节课回顾

(1) 定义：气块法中上升气块所获得的最大能量。

把浮力从自由对流高度（首次 $T_p > T_e$ ）积分到平衡高度（最后一次 $T_p < T_e$ ）所得的积分结果称为**CAPE**（Convective Available Potential Energy）。

$$\text{CAPE} \equiv \int_{z=\text{LFC}}^{z=\text{EL}} B dz$$

$$= g \int_{z=\text{LFC}}^{z=\text{EL}} \frac{T_p(z) - T_e(z)}{T_e(z)} dz$$

$$B \approx g \frac{T_p - T_e}{T_e}$$

①

正负面积之和

单位：J/kg 或  $\text{m}^2\text{s}^{-2}$



## 2.4 对流有效位能 CAPE

上节课回顾

### (2) 典型CAPE值

对流强度	CAPE (J/kg)	气块法预测的 $w_{max}$ ( $m s^{-1}$ )	可能的实际 $w$ ( $m s^{-1}$ )
弱-中等强度	< 1000	< 45	< 22.5
中-强	1000-3000	45-77	22.5-38.5
强-很强	3000-8000	77-126	38.5-63

# 2.4 对流有效位能 CAPE

## 上节课回顾

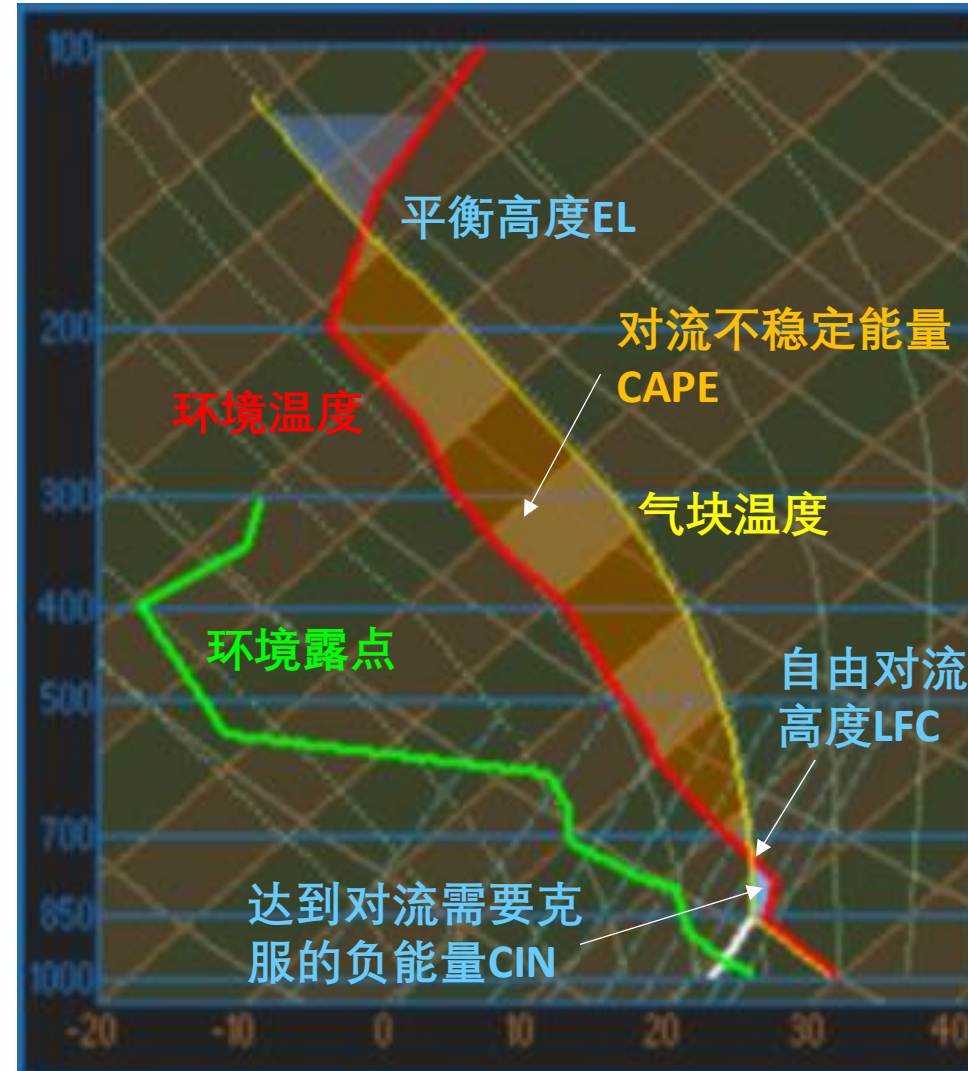
### 影响CAPE的因素:

环境减温率

绝热减温率

抬升气块选择

LFC和EL



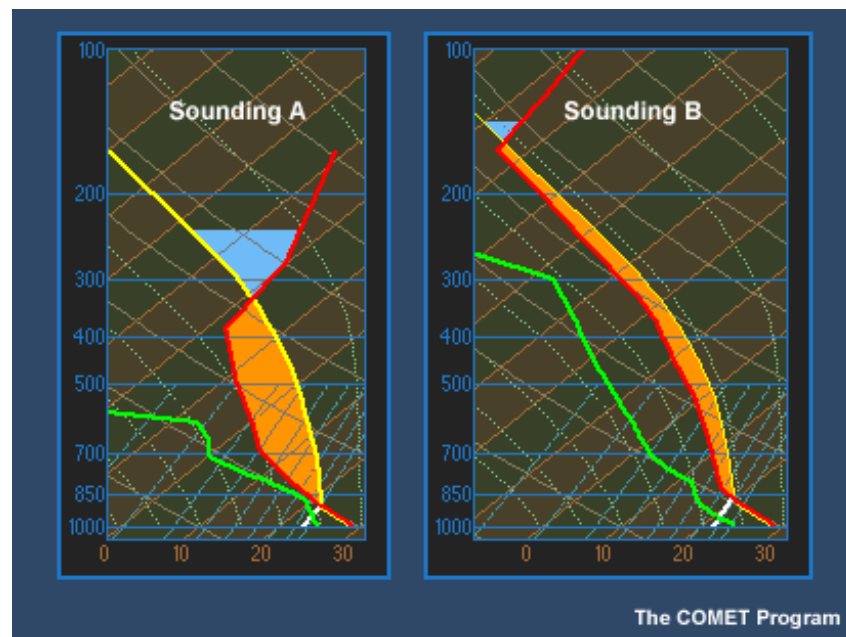
# (3) CAPE的分布特征对上升气流的影响



CAPE是浮力和积分厚度的函数，因而浮力的垂直分布对Updraft和风暴的强度有重要影响

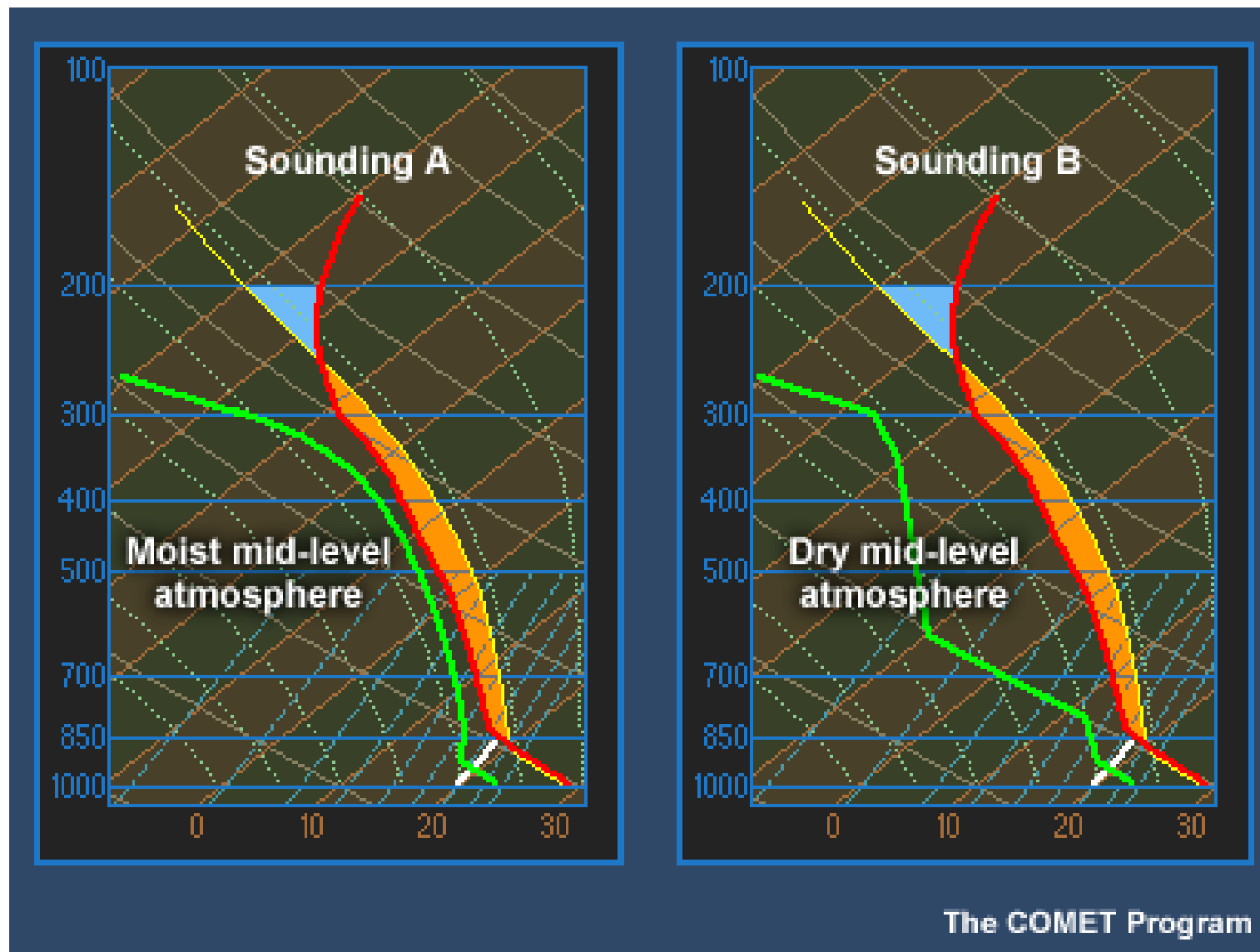
## 1) CAPE形状 细长型vs. 矮胖型

1a. CAPE 相同时干空气的卷入在细长型CAPE情况下对对流层中层的上升流比在矮胖型CAPE的情况有更加明显的减弱作用。干空气的卷入时间长，对浮力的减弱较明显。



强天气往往对应中低层的强上升流。

# 干环境下夹卷作用更明显





### 1b. 有关矮胖型CAPE与细长CAPE的雨滴的拖曳作用的差别

拖曳作用不取决于雨滴与地面的相对速度，而是雨滴与上升空气之间的速度差  
上升速度大的矮胖型CAPE背景下：

- 相对速度加大，向下的拖曳作用更大
- 大的上升速度环境中大粒子容易生成，也使拖曳作用加大。

上升气块因摩擦力被减小的速度计算  $f = ma = m \frac{dv}{dt}$

$$f dt = m dv$$

$$\int m dv = \int f dt = \int K v^n dt$$

摩擦力尼古拉兹曲线：

$$f = K v \text{ 层流区}$$

$$f = K v^2 \text{ 紊流粗糙区}$$

如果  $n = 1$ ,  $m \Delta v = K \Delta s$ , 细长型受拖曳较明显

$\Delta s$  为程长

如果  $n = 2$ ,  $m \Delta v = \int K v ds = K \bar{v} \Delta s$ , 与气层内的平均速度和程长之积成正比

2) NCAPE (对CAPE相对于积分厚度做归一化)

$$\text{NCAPE} = \frac{\text{CAPE}}{z_{\text{EL}} - z_{\text{LFC}}} = \frac{\text{CAPE}}{\Delta z} = \frac{\int_{z_{\text{LFC}}}^{z_{\text{EL}}} B dz}{\Delta z}$$

(Blanchard, 1998)

根据积分平均值定理, NCAPE实为 $\Delta z$ 厚度内的平均浮力

$$\text{NCAPE}|_{\Delta z} = \overline{B}|_{\Delta z} \quad \text{m s}^{-2}$$

2a. NCAPE是某一给定气层内的气块平均加速度的一个更直接的估计

$$\overline{\frac{dw}{dt}} = \overline{B}|_{\Delta z} = \text{NCAPE}|_{\Delta z}$$

$\Delta z$ 可以取任何值, 可以方便用于任一感兴趣气层内的平均浮力和气块加速度

2b. 具有相同CAPE的两个气团其平均浮力和上升流加速度可能差别很大

2c. NCAPE和对流强度的经验关系

NCAPE取值 ( $\text{m s}^{-2}$ )	上升流强度	CAPE形状
$\text{NCAPE} \leq 0.1$	弱上升流	细长
$0.1 < \text{NCAPE} < 0.3$	中等上升流	
$\text{NCAPE} \geq 0.3$	强上升流	矮胖

# (4) CAPE与气块的来源选择密切相关



## 1) SBCAPE (Surface based CAPE)

随着地面温度升高，对流一般会在午后起来，因而一般用预报的最高温度做温度订正

变率很大

高架对流时易低估CAPE

浅湿层时易高估CAPE

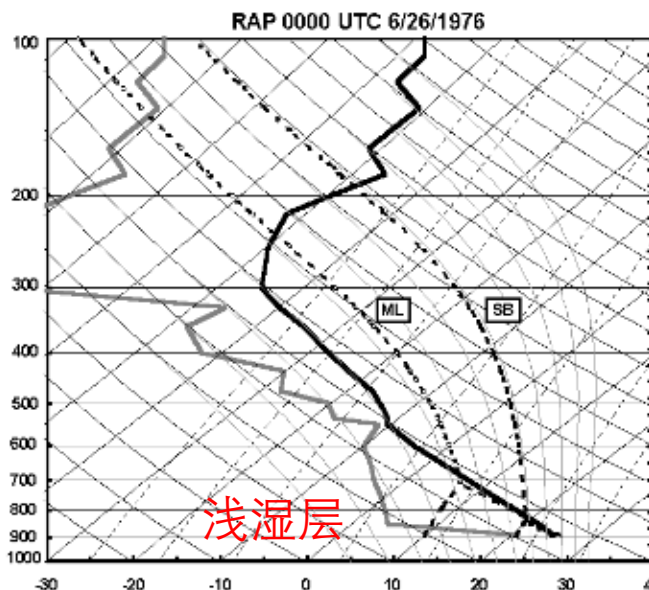
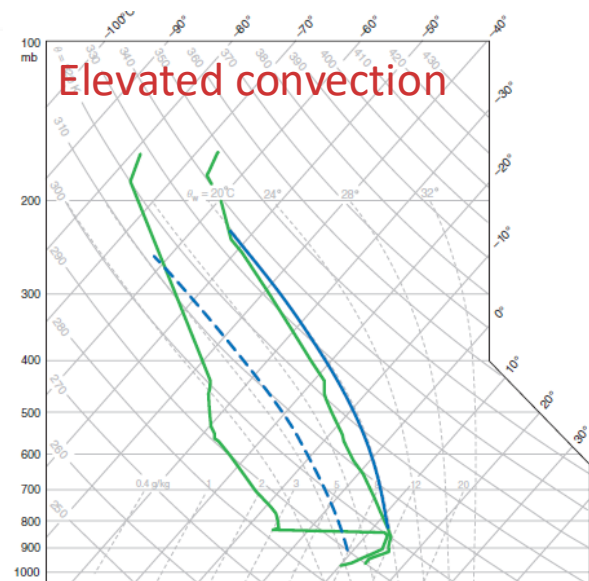
## 2) MLCAPE (Mixed layer CAPE)

气块始于平均层的中间位置

时空比较少变

有夜间浅层逆温时一般比SBCAPE大  
混合较好时与SBCAPE接近

浅层逆温或浅湿层时较好用。



# (4) CAPE与气块的来源选择密切相关

FNL: 地面-180 hPa的平均 $T$ 和 $T_d$

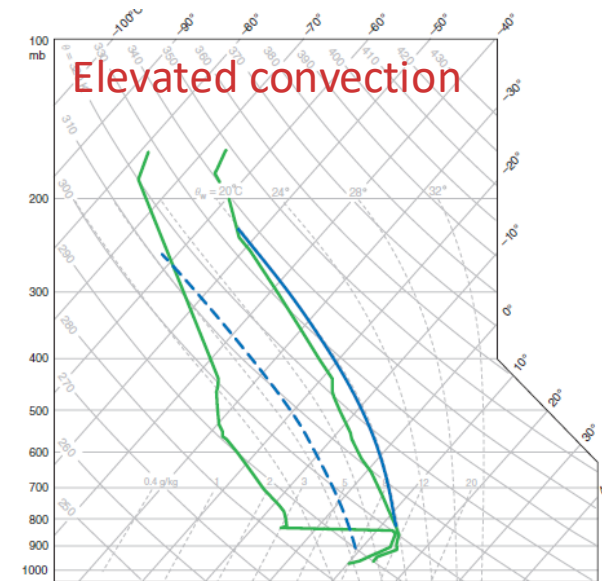
怀俄明学探空网站: 地面-500 m 的平均 $T$ 和 $T_d$   
(中国境内的站点于2019年1月20日被抹去)

## 3) MUCAPE (Most unstable CAPE)

在地面以上300 hPa层内找一个能得到最大CAPE的层次开始抬升

对高架对流较好用, SB、ML CAPE都会低估。

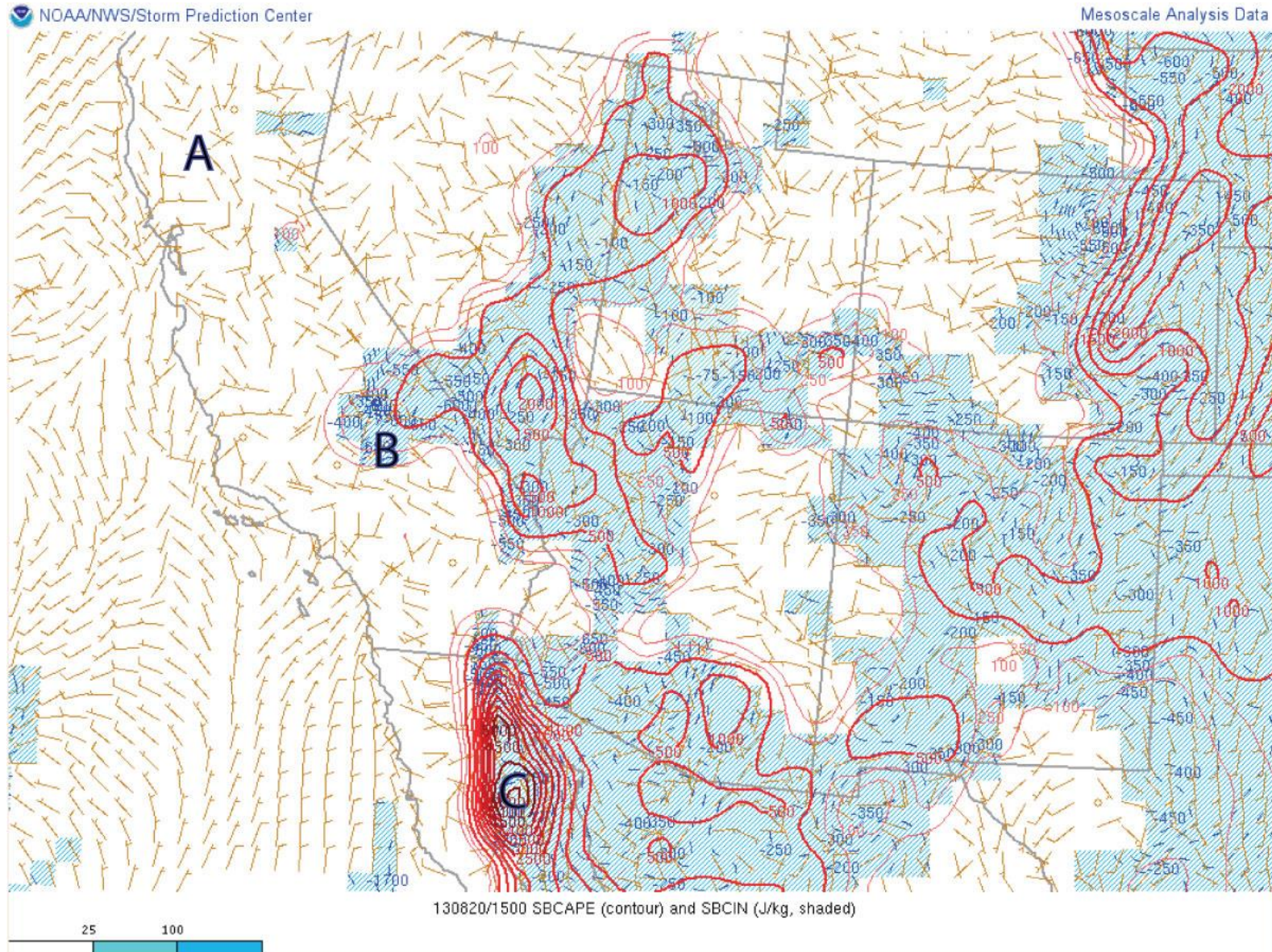
**ERA5: 地面到300 hPa高度层之间的最大CAPE**





# SBCAPE

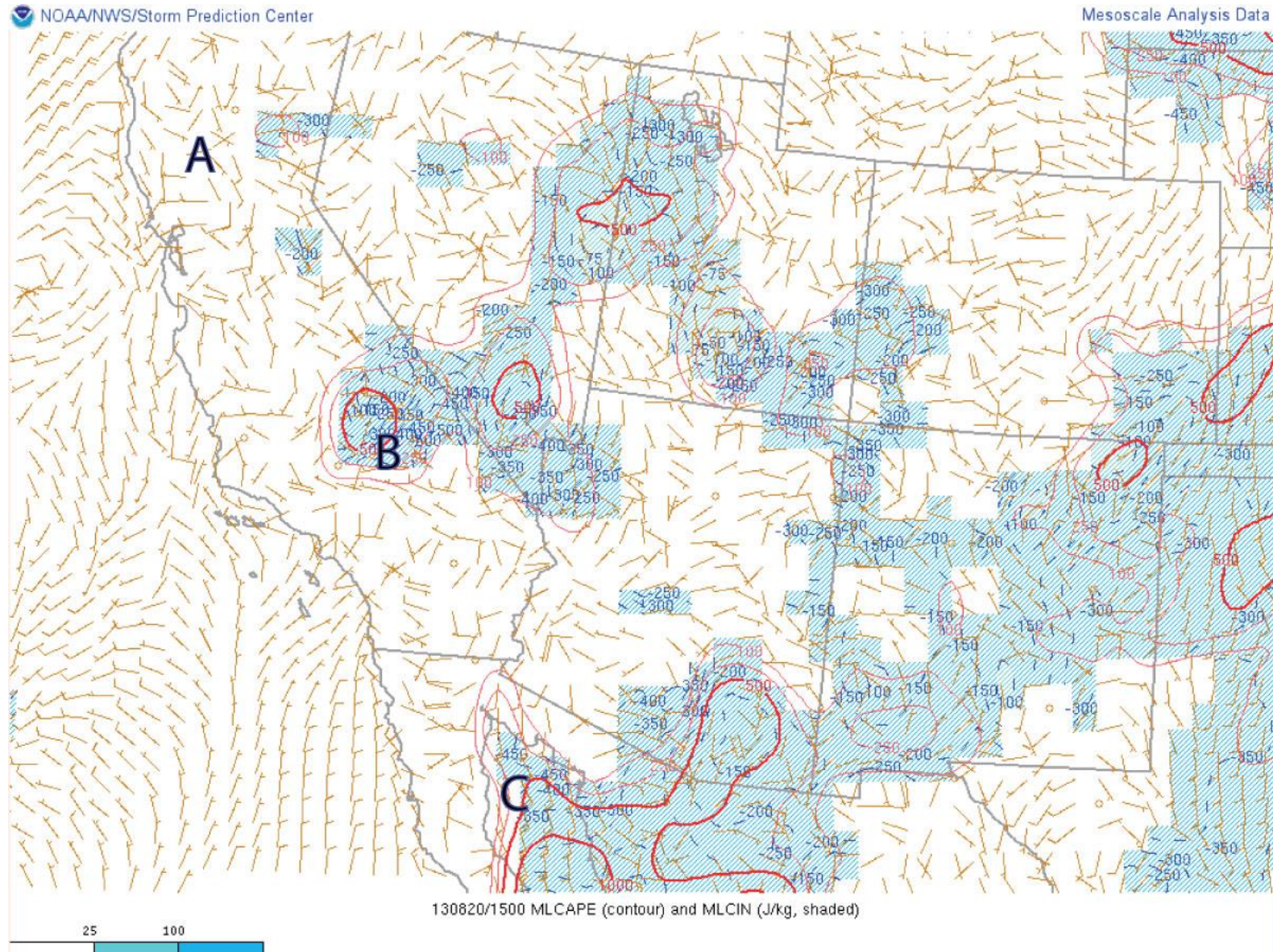
14 UTC 20 August 2013





# MLCAPE (the lowest 100 mb)

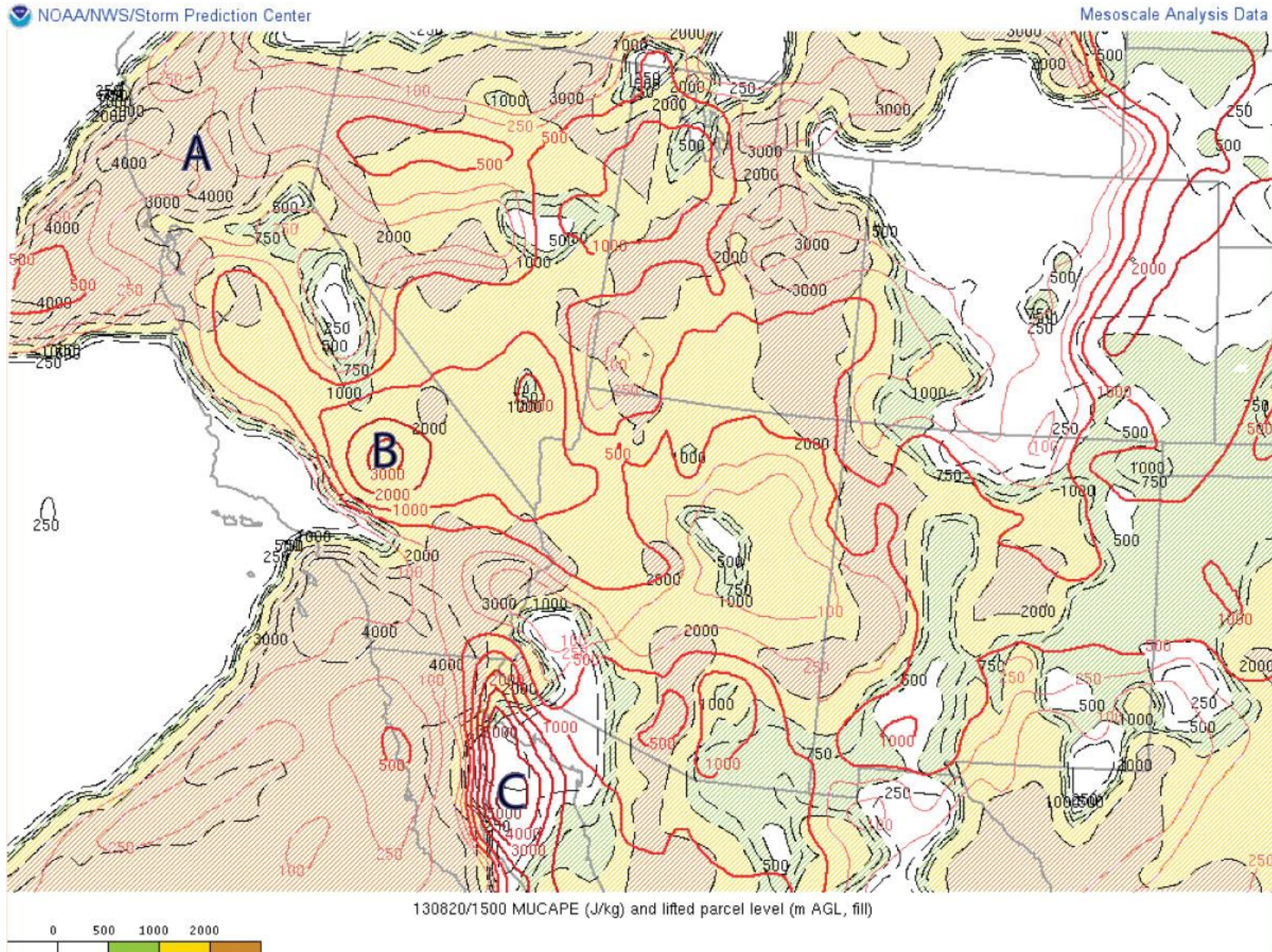
14 UTC 20 August 2013





# MUCAPE

14 UTC 20 August 2013





2012年7月21日下午2点的探空的CAPE,CIN和LCL.

	CAPE	CIN	LCL
	$\text{J kg}^{-1}$	$\text{J kg}^{-1}$	km
SB	2737	0	0.23
ML	746	-0.2	0.71

0-1 km AGL

## (5) 水汽对CAPE的影响 (虚温订正)

$$\text{CAPE}_v = \int_{z_{\text{LFC}}}^{z_{\text{EL}}} g \frac{(T_v)_p - (T_v)_e}{(T_v)_e} dz$$

$$\frac{B}{g} = -\frac{\rho_g'}{\bar{\rho}_g} \approx \frac{T_v'}{\bar{T}_v} - \frac{p'}{\bar{p}} - q_h$$

$$p = \rho R_d T_v$$

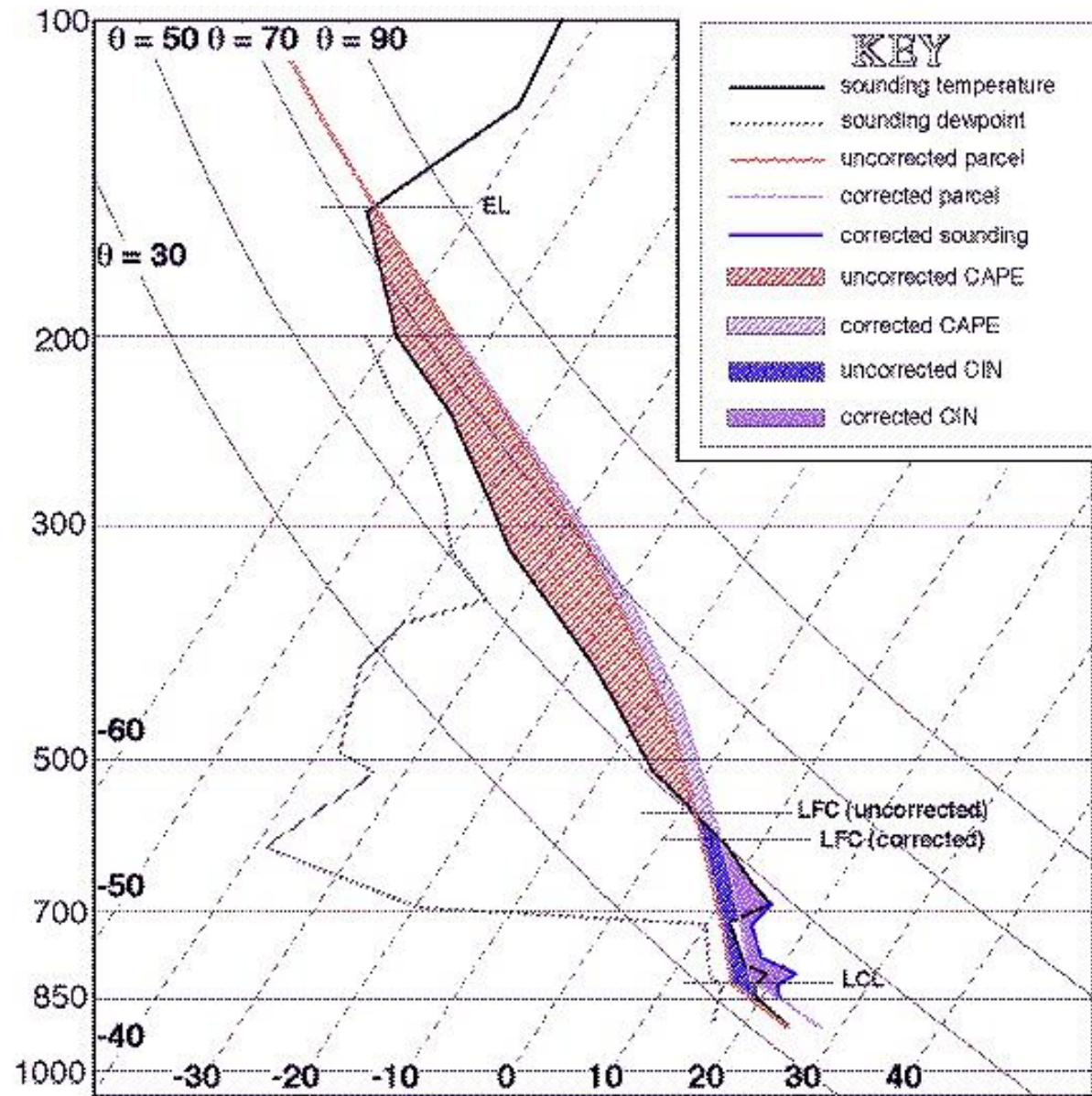
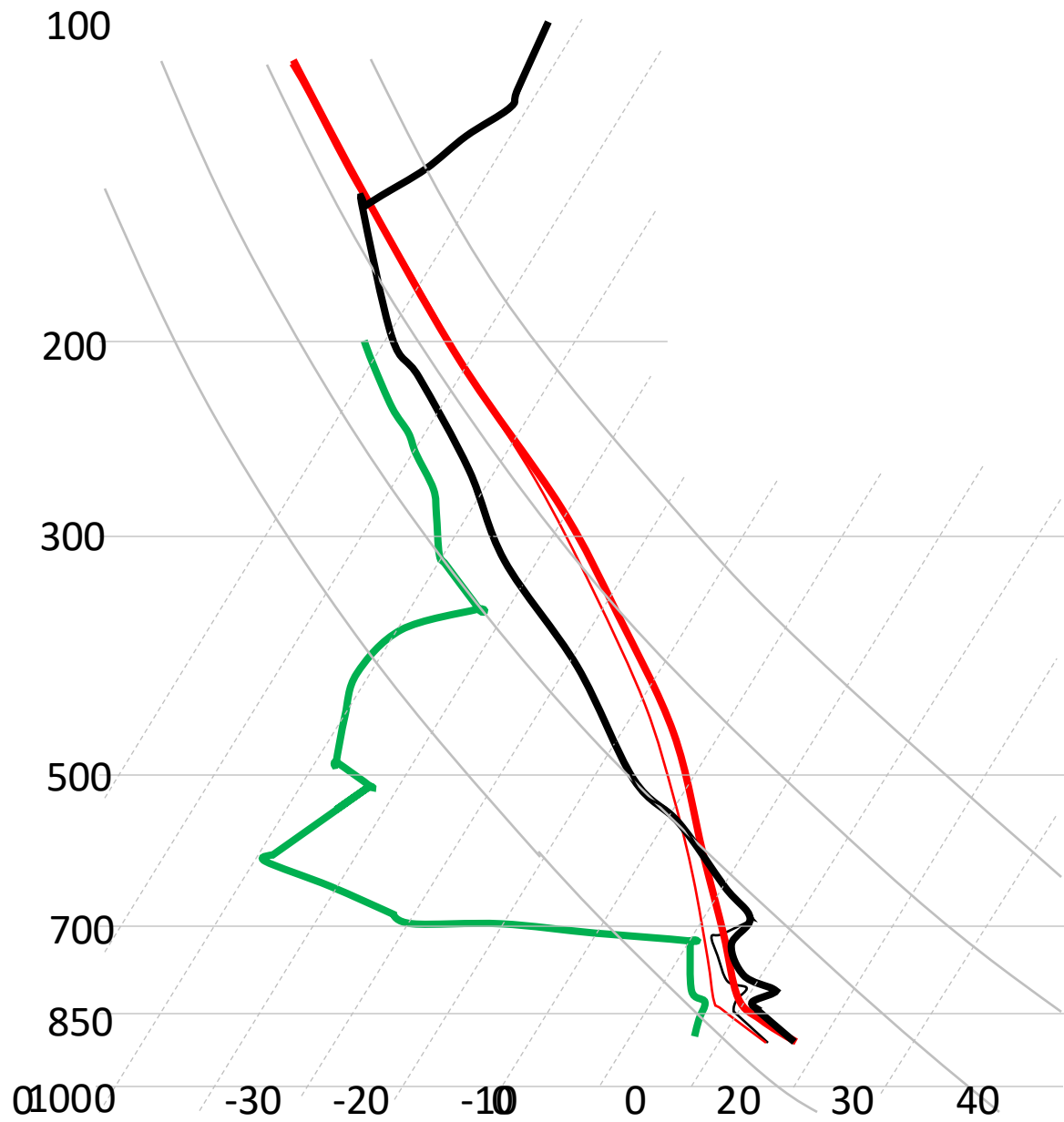
对湿空气，计算某一气压下的密度时，如果不调整 $R_d$ ，就需要用 $T_v$

$$T_v = T (1 + 0.608q)$$

订正步骤：

- 1) 基于原始的 $T$ 和 $T_d$ ，画出气块绝热曲线
- 2) 对环境温度和气块温度曲线做订正，湿度不做订正
- 3) 基于订正后的曲线得到 $\text{CAPE}_v$ 、 $\text{CIN}_v$ 、 $\text{LFC}_v$ 、 $\text{EI}_v$ ，但是不改变LCL

(On using the virtual temperature correction by Chuck Doswell; Doswell and Rasmussen, WAF, 1994)



## (5) 水汽对CAPE的影响 (虚温订正)



订正结果:

- 1)  $\Gamma_p$ 的订正幅度大于 $\gamma$ , LFC会降低, CAPE会增大。
- 2) 气块过了LCL就饱和了, 调整较大, 而环境一般不饱和, 调整较小。
- 3) **较小的CAPE, 虚温订正的相对差别较大**

# 2.5 稳定度指数

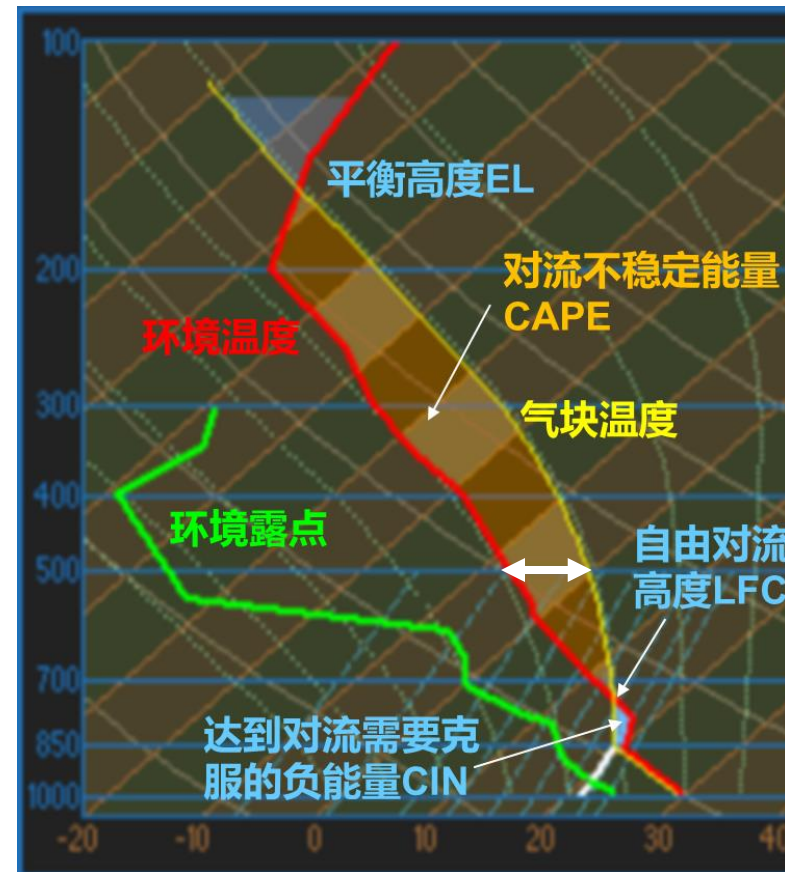
气块相对环境的温差，反映环境的稳定度，对流风暴发生的潜势  
常用的几个指数： LI 抬升指数， TT指数， K指数

## (1) LI (Lifting Index)

$$LI = (T_e - T_p)_{500 \text{ mb}}$$

单位： °C

负值表示不稳定  
反映CAPE的大小



# (1) LI (Lifting Index)

## Stability Index Summary Tables: LI

(extracted from AWS/TR-79/006, pp 5-41 to 5-42)

<i>LIFTED INDEX (LI)</i>	<i>THUNDERSTORM INDICATIONS</i>
> 0	Stable air; thunderstorms unlikely
0 TO -2	Weakly unstable, Thunderstorms possible – good trigger mechanism needed
-3 TO -5	Unstable – thunderstorms probable
< -5	Very unstable – strong thunderstorm potential with possibility of severe storms.

# (1) LI (Lifting Index)

Skew-T估计: 与如何抬升气块有关

## 1) SBLI

不适合高架对流, 比较适用于边界层混合较好的环境

## 2) MLLI

地面上50–100 hPa  $T$ 和 $T_d$ 的平均

## 3) BLI (Best LI)

地面–850 hPa 分小段抬升气块得到的最小值

## (2) Total – Totals Index (TT)

$$TT = T_{850} + T_{d850} - 2T_{500} \quad \text{单位: } ^\circ\text{C} \quad \text{均为环境温度}$$

$$= \underbrace{T_{850} - T_{500}}_{\text{Vertical totals}} + \underbrace{T_{d850} - T_{500}}_{\text{Cross totals}}$$

Vertical totals  
(VT)

与环境减  
温率有关

Cross totals  
(CT)

包含了低层  
水汽的作用

Note: 湿层在850hPa以下时不太好用, 不能反映水汽的作用



## (2) Total – Totals Index (TT)

### Stability Index Summary Tables: TT (East of Rockies)

(extracted from AWS/TR-79/006, pp 5-41 to 5-42)

<i>CROSS TOTALS</i>	<i>VERTICAL TOTALS</i>	<i>TOTAL TOTALS</i>	<i>EXPECT</i>
18-19*	26 or more*	44	Isolated or few thunderstorms
20-21	26 or more	46	Scattered thunderstorms
22-23	26 or more	48	Scattered thunderstorms, isolated severe thunderstorms
24-25	26 or more	50	Scattered thunderstorms, few severe thunderstorms, isolated tornadoes
26-29	26 or more	52	Scattered to numerous thunderstorms, few to scattered severe thunderstorms, few tornadoes
30	26 or more	56	Numerous thunderstorms, scattered severe thunderstorms, scattered tornadoes.

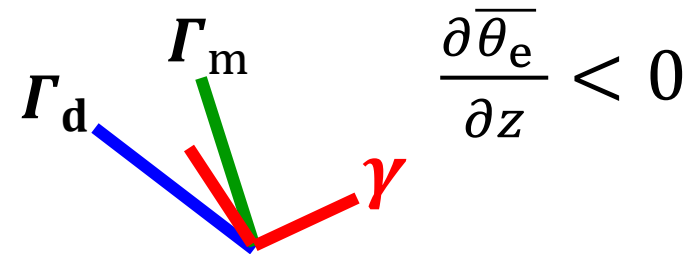
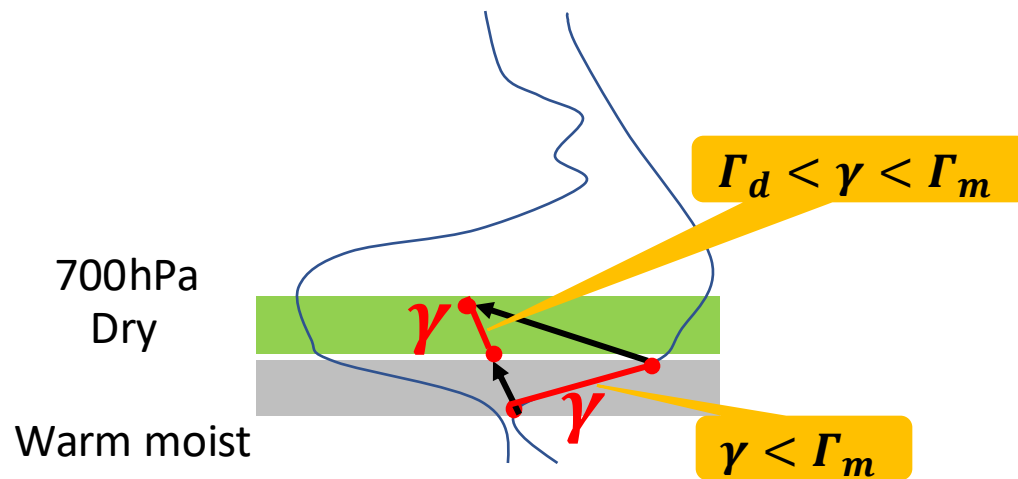
\*Except along Gulf Coast and over Gulf Stream where CT=16-19, VT>=23, TT=39

### (3) K指数

$$K = (T_{850} - T_{500}) + T_{d850} - (T_{700} - T_{d700}) \quad \text{单位: } ^\circ\text{C}$$

- 1) K指数基于850–500 hPa之间的环境 $\gamma$ 、对流层低层的水汽含量、湿层的垂直范围
- 2) 湿层在700 hPa以下不太适用

对于较小的K ( $<30$ )， $T_{700} - T_{d700}$ 可能很大，但700 hPa以下可能很湿，整层抬升可能发生对流，称为对流不稳定。



整层抬升，低层湿空气减温慢，高层干空气减温快， $\gamma$ 增大，导致不稳定

### (3) K指数



## Stability Index Summary Tables: K-index (East of Rockies)

(extracted from AWS/TR-79/006, pp 5-41 to 5-42)

<i>K-index (East of Rockies)</i>	<i>Airmass thunderstorm probability</i>
< 20	None
20 to 25	Isolated Thunderstorms
26 to 30	Widely scattered thunderstorms
31 to 35	Scattered thunderstorms
>35	Numerous thunderstorms

## 2.6 CIN (Convective Inhibition)



### (1) Capping Inversion

在地面湿层之上紧挨着的一个稳定层

由于这一层是绝对稳定的，这个盖子能够阻止气块达到LFC，因而阻碍对流的生成。

对流触发必须首先克服Capping Inversion



## (2) CIN (Convective Inhibition)



对流抑制：把空气块从地面抬升到LFC需要做的功。

用于描述Capping inversion的强度

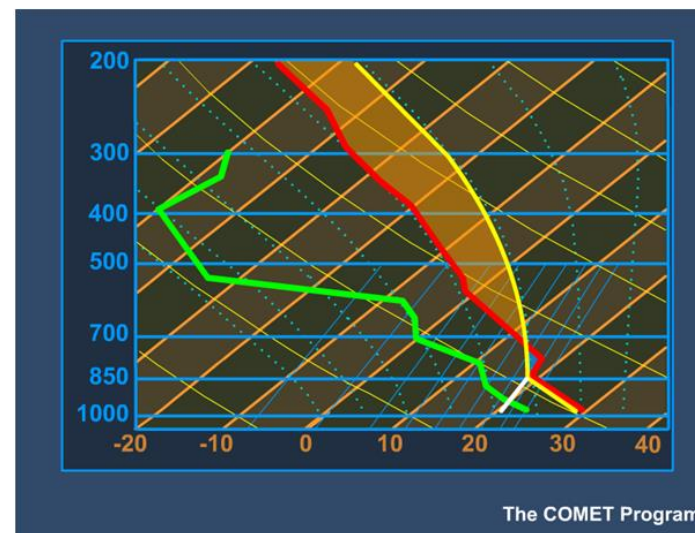
$$B \equiv g \frac{T_p - T_e}{T_e} \quad T_p < T_e, \quad B < 0, \text{ 气块下沉}$$

### 1) Skew-T计算

在Skew-T上，相当于环境温度廓线和从地面(sfc)到LCL的干绝热线与从LCL到LFC的湿绝热线之间的负面积。

数学上是负值，实际应用一般只提它的绝对值。

$$\text{CIN} \equiv \int_{z=\text{sfc}}^{z=\text{LFC}} B dz = g \int_{z=\text{sfc}}^{z=\text{LFC}} \frac{T_p - T_e}{T_e} dz$$



## (2) CIN (Convective Inhibition)



### 2) CIN的取值与风暴发生的对应关系

<b>CIN*</b> (convective inhibition)	<50	weak cap that can be easily broken by surface heating
	50 to 200	moderate cap that can be broken by strong heating/synoptic scale forcing
	>200	strong cap that impedes thunderstorm development

## (2) CIN (Convective Inhibition)

### 3) 大气克服CIN或Capping Inversion的方法

增温



## (2) CIN (Convective Inhibition)

### 3) 大气克服CIN或Capping Inversion的方法

增湿 (改变LCL)





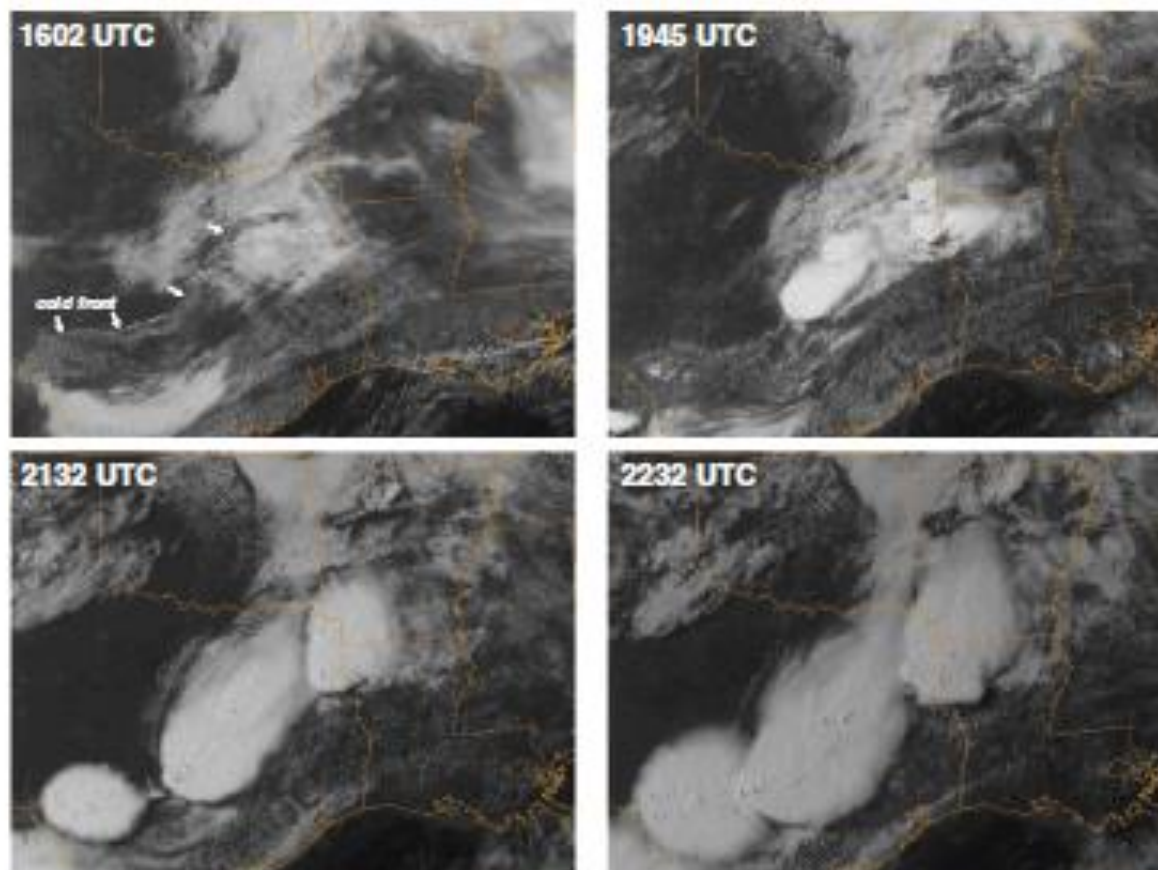
## (2) CIN (Convective Inhibition)

### 3) 大气克服CIN或Capping Inversion的方法

天气尺度抬升(锋面)



## 锋面抬升触发对流个例

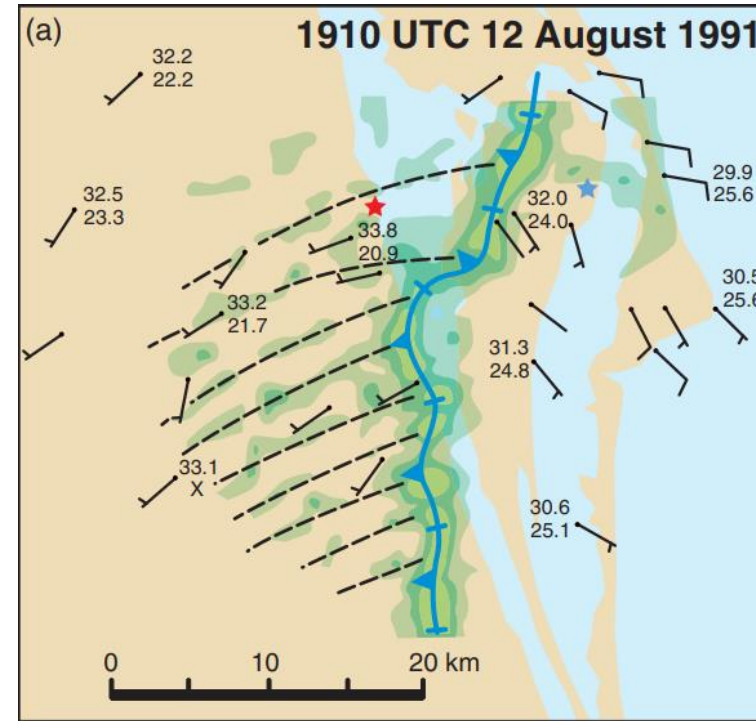
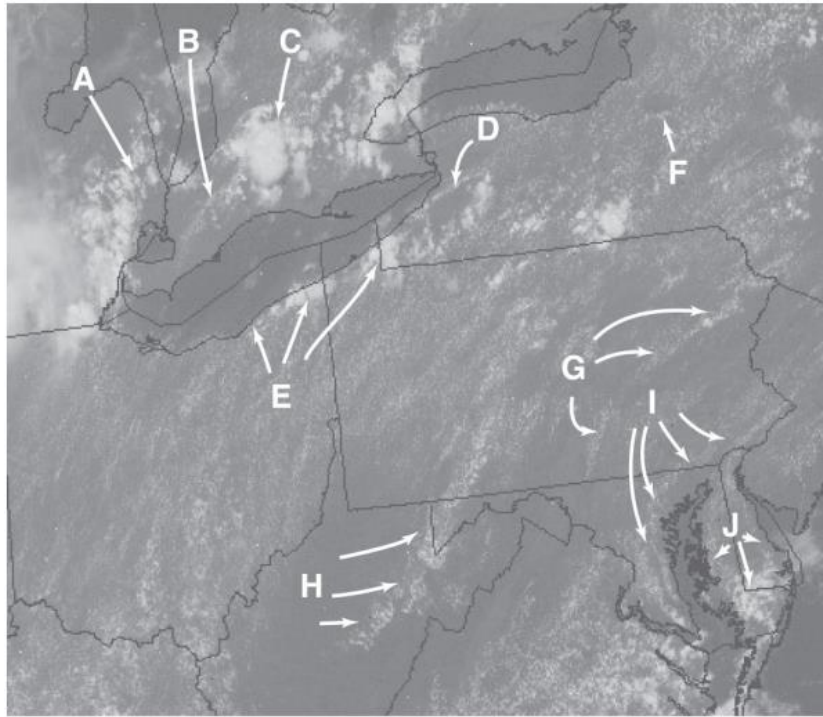


**Figure 7.2** In the absence of favored topographic features that act as elevated buoyancy sources, DMC tends to be initiated along air mass boundaries, which are usually accompanied by a wind shift and convergence. This allows forecasters to enjoy at least modest predictability with regard to anticipating the location of convection initiation, for such boundaries are fairly easily observable in routinely available synoptic surface observations and radar and satellite data. The sequence of visible satellite images shows the development of a line of severe thunderstorms along a cold front on 27 May 1997. The town of Jarrell, TX, was devastated by a tornado during this event.

## (2) CIN (Convective Inhibition)

### 3) 大气克服CIN或Capping Inversion的方法

中尺度抬升(干线、海陆锋、地形、山谷锋等)





## (2) CIN (Convective Inhibition)

### 4) 克服CIN需要的抬升速度估计

$$w = \sqrt{2|CIN|}$$

### 5) CIN对强对流天气的作用

有逆温层存在时，白天在增温增湿的情况下，有利于不稳定能量的累积增大，因而对流可能会比没有Cap时更强，更剧烈。